



# Council of Northern Caving Clubs

## Reports for Annual General Meeting 2012

### **Secretary's report**

From a secretarial perspective there is very little to report as very little has happened since the last CNCC committee meeting.

The CNCC treasurer discussed with me whether or not CNCC was subject to tax on the profits that we make. I have spoken with my accountants regarding this matter and there are a number of possible ways forward.

CNCC can pay full tax on its income and tax on its interest in bank accounts. Or, the most beneficial to CNCC, would be to become a conservation charity. This does not require registration, but will involve some changes in the wording to the constitution. Looking at the documents that I have currently seen, we are already in effect a conservation charity that being an organisation that spends its income on conservation work in the community and is run by volunteers.

At this moment in time I do not have all the facts, nor do I fully understand some of the compliance. What I propose, is that throughout 2012 I present facets of the conservation charity status at meetings, this we can digest in small chunks with the aim of making a decision on some constitutional word changes and take on conservation charity status at the 2013 AGM.

Having this status will also mean that we will not pay tax on the interest that CNCC accrues in the high interest account as we will have HMCR exemption.

Whatever we decide it will need to be debated throughout 2012 as the question has been raised.

### **Access Officers' report**

There have been no changes to any of the access arrangements that have not been reported to the CNCC committee throughout the year.

After a discussion with the BCA training officer it has become apparent that cave instructors (CIC's) are using their clubs permits to deliver training and assessments for the CIC scheme on behalf of BCA. To avoid any insurance implications in the event of an incident during these training and assessments; I propose that the committee accepts the following procedure. For CIC's delivering training or assessments under the BCA CIC scheme, the BCA training officer will contact the CNCC Access Officer with the date and location of the training, the access officer will then contact the relevant meets secretary who will issue the permit to the access officer who will then pass it on to BCA training officer. This procedure is only for CIC's operating in the north and is not open to the LCMLA scheme.

**CNCC Technical Group**

I have been informed by the MD of Bolt Products that the production of 2000 anchors is under way and should be available for delivery end of February/March 2012.

I have appended to this report the document which outlines the testing that was undertaken throughout the year by BCA Equipment & Techniques Committee and the CNCC Technical Group with the amendment that was noticed at the last CNCC committee meeting.

**BCA Equipment & Techniques Committee**

There is nothing to report as there has not been a meeting since the last CNCC meeting. The next meeting is 18 March 2012.

**Training Officers report**

Due to my current work load for cavers and the CNCC I have been unable to fulfil this role during 2011. However, it is a role that I fully believe CNCC should undertake and I will try and run an event during 2012-2013. If any clubs want any training there is grant aid available from BCA provided they have a BCA CIC delivering the training. There may also be provision for CNCC to access grant aid from BCA, if this becomes the case I will run a rescue course for club trainers during this summer.

In the mean time if clubs have a designated training person could that person contact me so that I can initiate a forum to discuss club training and training delivery.

If any clubs want to run a training event and want advice send me an email I will be more than happy to get involved.

I am more than happy to be re-elected to any or all of the roles that I currently do. However, if there is a willing volunteer who wants to further their career and undertake any of the roles, then I am more than happy for that person to be elected.

Les Sykes

CNCC secretary

CNCC Training Officer

CNCC Access Officer

CNCC co-representative BCA Equipment & Techniques Committee



## Anchor Tests 2011

### Scope

This report details the complete series of anchor tests designed to find a replacement for the DMM Eco anchor carried out by the BCA Equipment & Techniques Committee during 2011.

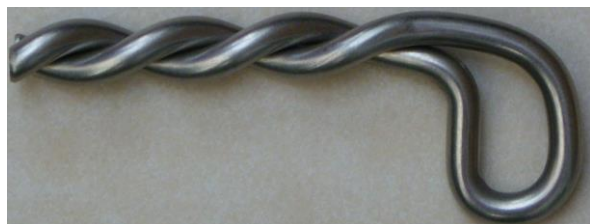
### Introduction

Following the cessation of production of the DMM Eco anchor it became necessary to source a replacement which would fulfil all the criteria decided by the Committee during their consultative process. The main requirement was that the anchors should attain an axial load of at least 25kN before failure. The logic for this standard was that most, if not all, of the other components in the equipment safety chain would have failed at this loading. As the vast majority of natural caves are in carboniferous limestone it was decided that the initial tests would be carried out in this substrate.

An identical looking product to the DMM anchor was offered by Jonathon Sims who had manufacturing contacts in China. An initial test batch of 200 anchors was acquired and designated "Peco Batch 1". Subsequently, a further production batch of 2000 anchors was ordered designated "Peco anchor Batch 2". As will be observed later in the report, four out of a sample of sixty four Batch 2 Peco anchors suffered catastrophic metallurgical failure below the 25kN threshold.



Further research identified another possible alternative supplied by Bolt Products manufactured in Germany to BS EN 959. The major difference with this anchor is that whilst it was still made with 8mm 316 stainless steel bar the two tangs of the anchor were twisted unlike the parallel bars of the Eco and Peco anchors. Another difference was that the eye of the anchor was slightly smaller than the Eco and Peco anchors although it was still of adequate size.



## Method

All anchors were tested in batches of 32. The two types of chemical anchor mortars (i.e. resins) that were used for installing the anchors were RAWL R-KER Epoxy Acrylate Styrene free resin manufactured by RAWL fixings and Allgrip KMR-RES resin which is manufactured by Exchem UK. This is the unsaturated polyester resin in styrene that has been previously used for the setting of Eco anchors.



Test 1 - Peco Anchor Batch 2 – Allgrip KMR-RES - Horseshoe Quarry - Stoney Middleton

Test 2 - Peco Anchor Batch 2 – Allgrip KMR-RES - Ingleton Quarry

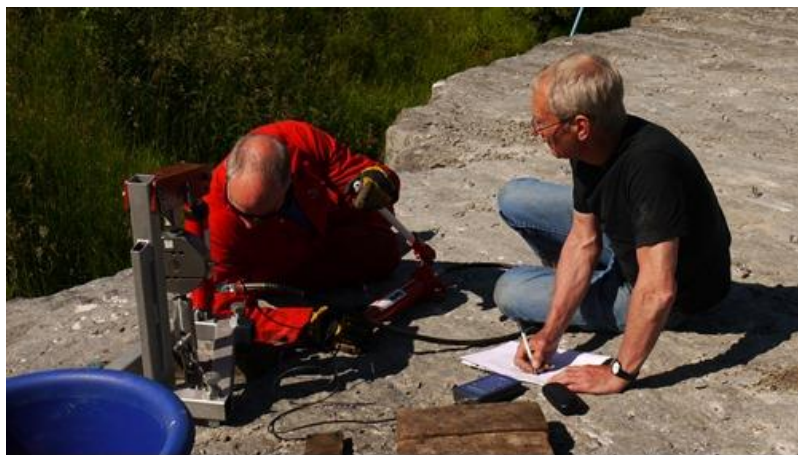
Test 3 – Peco Anchor Batch 1 – Allgrip KMR-RES - Ingleton Quarry

Test 4 - BP Anchor - RAWL R-KER - Ingleton Quarry

Test 5 - BP Anchor – Allgrip KMR-RES - Ingleton Quarry

See Appendix 1 - Test 1 (Purple) - Test 2 (Red) – Test 3 – (Green) – Test 4 – (Blue) – Test 5 - (Black)

All the anchors were installed in carboniferous limestone in compliance with the BCA E&T Committee document "Permanent Resin Bonded Anchors – Installation Procedure, Training and Documentation" (IPTD); which is the same as the recommend procedure by both resin manufacturers. The Peco anchors were installed into holes 18mm diameter x 100mm deep. The Bolt Products anchors were installed into holes 16mm diameter x 100mm deep. The holes in Ingleton Quarry were cleaned using water (pressure wash), brushed and washed until all the limestone dust had been removed. They were then dried using absorbent cloth. The holes in Horseshoe Quarry were dry cleaned using a brush and a blower until all the limestone dust had been removed.



## **Results**

**Test date: 24th June 2011**

**Anchor type: Peco Batch 2 (production batch)**

**Resin: KMR-RES**

**Location: Horseshoe Quarry - Stoney Middleton**

**Substrate – Black Layer – Stoney Middleton Sequence**

During the test period it became apparent that the substrate was not as uniform or as structurally strong as was initially thought. There were areas where the thin substrate microstructure caused some placements to fail prematurely with resultant delamination. However, even with substrate failure the tests did indicate that the anchor placement system would give reasonable test results in thinly bedded and relatively weak bituminous limestone strata. More concerning was that two Peco anchors failed by fracture of the metal at the lower curvature of the eye. The load at deformation was consistent within a range of 10-16kN giving a mean of 13.6kN. The ultimate failure load i.e. the peak load at which the anchor started to egress from the resin or the load required to extract the anchor from the resin, whichever was higher, was within the range 16-35kN with a mean of 27.44kN. Although the fracturing of the substrate did result in some low readings the mode of failure was consistently the anchor to resin bond except for the two anchors which fractured at the lower curvature of the eye. Peco anchors No. BCA 0182 and BCA 0004 suffered catastrophic metallurgical failure at 26kN and 16kN respectively.

**Test date: 28th June 2011**

**Anchor type: PECO Batch 2 (production batch)**

**Resin: KMR-RES**

**Location: Ingleton Quarry**

**Substrate – Yorkshire Limestone**

32 Peco anchors were randomly selected from the remainder of the batch and set in structurally solid limestone. As there was only one small area of the test bed where substrate failure occurred the results were generally in line with expectations. However, as in the test at Horseshoe Quarry, two Peco anchors fractured at the lower curvature of the eye. The load at deformation was consistent within a range of 11-15kN giving a mean of 13.28kN. The ultimate failure load, as described above in the tests at Horseshoe Quarry, was within the range 14 - 47kN. Giving a mean peak load force of 33.22kN. Although the fracturing of the substrate did result in some low readings the mode of failure was again consistently the anchor to resin bond except for the two anchors which fractured at the lower curvature of the eye.

Peco anchors No. BCA 0069 and BCA 0153 both fractured at 18kN and 14kN respectively. The main concern is that the lowest fracture load (14kN) would technically make the anchor placement the weak link in the rigging system. The anchor in the photograph was cut to remove it from the placement.



**Test date: 24th September 2011**

**Anchor type: Peco Batch 1**

**Resin: KMR-RES**

**Location: Ingleton Quarry**

**Substrate – Yorkshire Limestone**

During the test period it became apparent that the chemical anchor mortar had not thoroughly mixed during application into the hole. This resulted in two relatively low readings. Anchor test number 10 was extracted at 26kN. and anchor test number 13 was extracted at 18kN. On closer inspection of the chemical mortar it was found to be granular which could indicate that thorough mixing had not occurred or that the resin required a longer curing time. The load at deformation was consistent within a range of 14-18kN giving a mean of 16.3kN. The ultimate failure load i.e. the peak load at which the anchor started to egress from the resin or the load required to extract the anchor from the resin, whichever was higher, was within the range 18-45kN. with a mean of 34kN.

**Date: 22nd October 2011**

**Anchor type: Bolt Products 8mm x 100mm twisted stainless steel anchors**

**Resin: RAWL**

**Location: Ingleton Quarry**

**Substrate – Yorkshire Limestone**

Thirty three Bolt Products anchors were installed in limestone (somebody couldn't count). During the test period it became apparent that the chemical anchor mortar had not thoroughly mixed during application into one of the holes. The peak load to remove this anchor was 36kN. RAWL have been contacted and from the information supplied by us have initiated an investigation. The failure mode is initially similar to a DMM Eco anchor with elongation of the eye towards the direction of the applied load. However, unlike an Eco anchor as it is extracted from the substrate the anchor twists, and along with it the load cell, until the load is released as the anchor suddenly and violently egresses from the resin. The load then gradually increases until the anchor starts to twist and the process is repeated. This behaviour continues until the anchor is extracted from the substrate. Generally the anchor's failure range was consistent; however anchor





test numbers 20 and 26 were below 30kN. As the failure mode is anchor to resin bond this is probably due to poor mixing and adhesion of the resin. The deformation range was 18-23kN. The ultimate failure load i.e. the peak load at which the anchor started to egress from the resin or the load required to extract the anchor from the resin, whichever was higher, was within the range 24 - 47kN with a mean of 35.5kN. From the data gathered from these tests it is evident that the anchor and peak load forces are consistent and similar to the DMM Eco and Peco anchors.

**Test date: 2nd November 2011**

**Anchor type: Bolt Products 8mm x 100mm twisted stainless steel anchors**

**Resin: KMR-RES**

**Location: Ingleton Quarry**

**Substrate – Yorkshire Limestone**

As a consequence of the high pull out loads experienced during these tests the mode of failure changed. Normally, in Eco & Peco anchors, the mode of failure is the anchor to resin bond. The Bolt Products anchors, in the majority of cases, experienced substrate failure and the resin/rock bond with it. On a number of the tests cone fracture and delamination of the substrate occurred followed by the failure of the resin to rock bond. However, as demonstrated in the photo opposite even with delamination the anchor placement still held 51.73kN. With the reduced hole size (16mm) the amount of resin in the placement is also reduced. This causes the resin to fragment and become almost pulverised by the load during extraction of the anchor. This pulverisation is more evident lower down in the placement.



An interesting observation was that the anchors were still holding only a little less than their peak loads when half to two thirds of their length had been extracted. In comparisons between the RAWL R-KER and the Allgrip KMR-RES the inclusion of styrene in the formulation means failure loads are 10kN higher with the Allgrip KMR-RES resin.



Another interesting observation was that the shank of the Bolt Products anchor unwound and elongated under loads approaching 50kN. (5<sup>th</sup> anchor from right picture below). The deformation loads

were similar to the previous test. The ultimate failure load i.e. the peak load at which the anchor started to egress from the resin or the load required to extract the anchor from the resin, or substrate failure, whichever was higher, was within the range 32 - 63kN with a mean of 44.91kN.



## Conclusions

From the data gathered from these tests it is evident that the combination of the Bolt Products 8mm twisted stainless steel bar anchor and the Allgrip KMR-RES produces strength well in excess of both the Eco and Peco anchors. Also Allgrip KMR-RES is far superior to the anchor manufacturers recommended resin. The reason the anchor manufacturer specifies the RAWL R-KER resin is that in Germany the use of styrene based resins is illegal for Health and Safety concerns. There is no such restriction in the UK.

The graph of ascending extraction loads in Appendix 2 demonstrates the difference in peak load force between the Bolt Products anchors installed with RAWL fixings resin and Allgrip KMR-RES. The graph of ascending extraction loads in Appendix 3 shows the comparative extraction loads of the two batches of Peco anchors and in Appendix 1 a comparison of all five test series.

## Future Objectives

1. To test a number of the Bolt Products anchors with KMR-RES in shear (radial).
2. To conduct tests of anchor strengths in other weaker substrates as defined by the Equipment and Techniques Committee.

Anchor installation team: R.S. Dearman, L. Sykes, G. Jones, S. Sykes

Anchor test team: R.S. Dearman, L. Sykes, G. Jones, S. Sykes, S. Dale

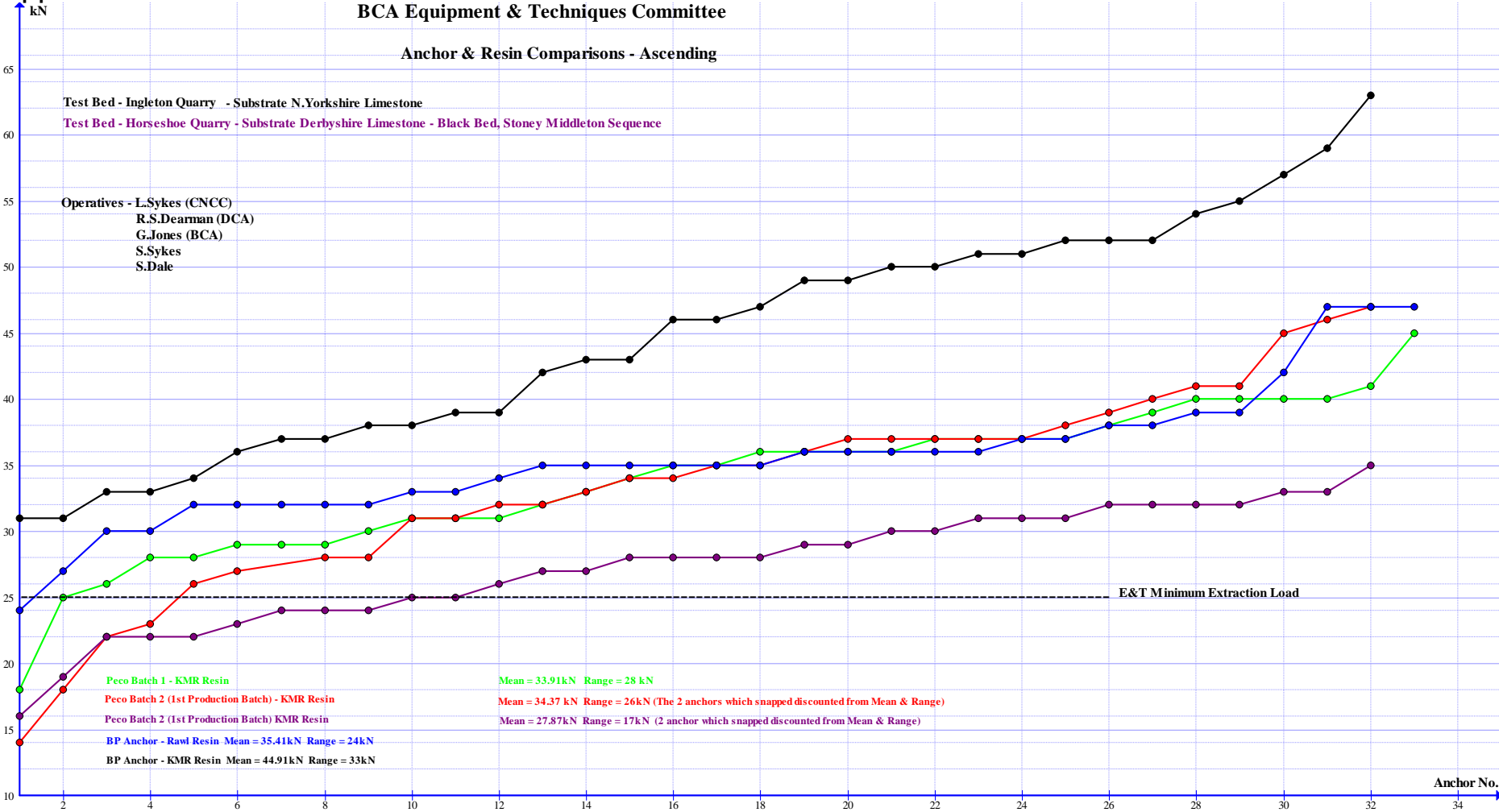
**Report compiled by L. Sykes, R.S. Dearman**

Photographs: G. Jones, L. Sykes

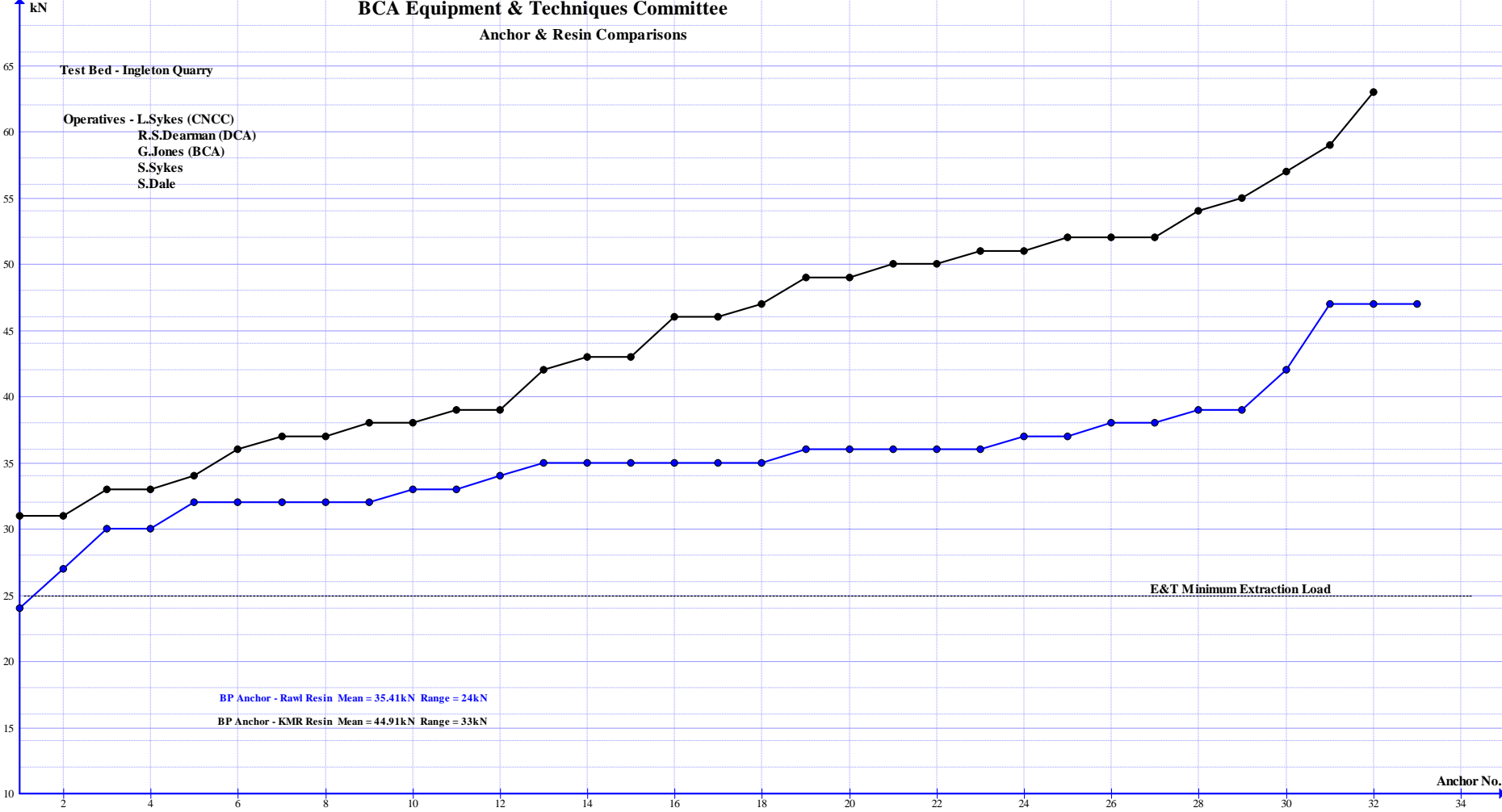




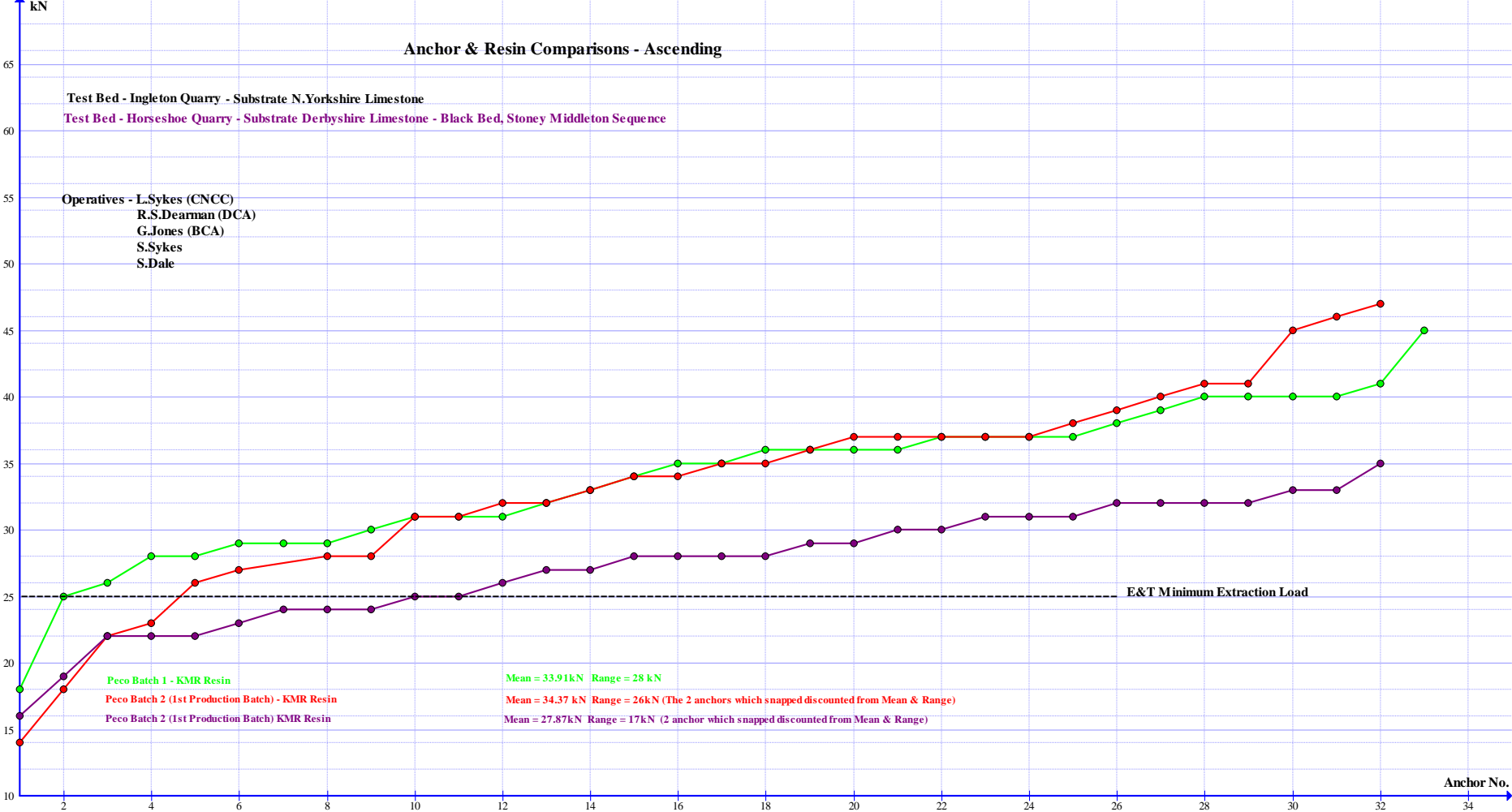
Appendix 1



Appendix 2



Appendix 3



# **Meets Secretary's report for Birks Fell, Robinsons Pot and Mongo Gill**

## **General**

This is my 23<sup>rd</sup> year as access controller and I know of no problems regarding access to Birks Fell, Robinsons Pot or Mongo Gill

## **Birks Fell**

A year ago the National Trust informed me that, although they wished the access agreement to continue under the same conditions as now, they wished to see a more formal agreement drawn up in a similar way to Robinsons Pot. Since then I have heard nothing and the staff involved have all left. I have received 7 requests for permits for 2012, the same number as for 2011 at this time.

1977	22	1978	35	1979	40	1980	41	1981	50
1982	47	1983	52	1984	63	1985	46	1986	55
1987	44	1988	28	1989	32	1990	25	1991	41
1992	49	1993	35	1994	41	1995	39	1996	34
1997	35	1998	28	1999	32	2000	15	2001	0
2002	21	2003	27	2004	10	2005	12	2006	15
2007	17	2008	15	2009	10	2010	13	2011	12

Average number of permits per year for the last 10 years is 15 (15)

## **Robinson's Pot**

After some difficulties the new agreement with the National Trust was finalized. It allows a maximum of 5 permits per year on the second Saturday of each month, June to October inclusive. Five requests for permits have been received, 2 from Clubs who have never had a permit and three from clubs who have previously held a permit. I propose that there is no need for a ballot and I simply issue the permits to these clubs.

## **Mongo Gill**

The new access agreement with no closed season but no access on Bank Holiday Weekends appears to be causing no problems. One trip down Valentines Hole (the first for 8 years) had to be abandoned when the lock would not open. I have recently removed this padlock and the landowner has replaced it. This should enable the rescheduled visit for later this year to take place. So far no permits have been requested for Great Expectations, one was issued last year. The connection with Stump Cross stream way remains well and truly blocked by a major collapse.

1981	28	1982	39	1983	39	1984	44	1985	24
1986	28	1987	29	1988	36	1989	38	1990	38
1991	36	1992	43	1993	34	1994	36	1995	20
1996	26	1997	0	1998	0	1999	22	2000	22
2001	5	2002	5	2003	3	2004	9	2005	6
2006	10	2007	6	2008	8	2009	10	2010	3
2011	8								

Average number of permits per year for the last 10 years is 7(6)

***Ric Halliwell  
15 February 2012***